

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE
APPLICATION FOR UNITED STATES LETTERS PATENT

for

IMPROVED STREAM SWITCHING SYSTEM

by

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IMPROVED STREAM SWITCHING SYSTEM

1 CROSS-REFERENCE TO RELATED APPLICATIONS

2 This application claims priority to provisional application 60/141,357 filed June 28, 1999.

3 STATEMENT REGARDING FEDERALLY SPONSORED 4 RESEARCH OR DEVELOPMENT

5 Not Applicable.

6 BACKGROUND OF THE INVENTION

7 It is often very important to know what fluids are flowing through a conduit such as a
8 pipeline. For example, a buyer and seller may agree upon a price for the fluid flowing through a
9 process pipeline based upon the content of the fluid stream. Thus, the fluid content must be
10 measured. Where multiple pipelines are positioned near one another, it may be economical to use a
11 single meter or measurement device to monitor all of the fluid flows. The device used to extract and
12 deliver the fluid to the measurement device is traditionally referred to as a sampling system.

13 Figure 1 includes a stream sampling system ("sampling system") 100. Although only a
14 single pipeline is shown, it is to be understood that multiple pipelines may be present. Sampling
15 system 100 includes a sample point attached to pipeline 110, an analyzer 130, and tubing 120 from
16 the sample point to the analyzer 130. Analyzer 130 may include a stream switching system 140 and
17 gas chromatograph 150. In operation, fluid flow through a process pipeline 110. The sample point
18 (preferably a probe fluid) obtains a sample of fluid and delivers it to analyzer 130 via tubing 120.
19 Analyzer 130 measures the content of the fluid sample and either returns the sample to the pipeline
20 or vents the sample to the ambient environment.

1 One problem with such a layout is the large distance from the analyzer 130 to the pipeline
2 110, which creates a large “dead volume” of fluid. Increased dead volume results in undue mixing
3 of consecutive fluid samples. This mixing of fluid samples results in “carry-over” between samples
4 for gas chromatograph analysis. Carry-over is undesirable because accurate analysis requires that
5 the analysis is representative of the fluid in the process pipeline. Since the volume of transport
6 tubing and stream sampling components must be flushed a minimum of ten times to insure a
7 representative sample, the “dead volume” results in significant lag time between sample analysis.
8 Therefore, upon a sampling of fluid from the pipeline 110, the “dead volume” of fluid must be
9 vented or otherwise disposed of before the new sample can be measured at the analyzer 130.
10 Further, although the magnitude of the “dead volume” could be reduced by placing the analyzer 130
11 closer to the sample point 110, regulations and safety concerns mandate a minimum 50 feet distance
12 between them. If placed closer than 50 feet from the pipeline 110, the analyzer 130 must be
13 contained in an expensive explosion-proof housing.

14 Figure 2 includes a stream switching system 140 attached to an analyzer oven 250 that is
15 part of gas chromatograph 150. Three pipes or tubes 210, 220, 230 attach to switching system 140,
16 and correspond to first, second and third flow paths. The first pipe or tube 210 connects to a first
17 sample point 212 and carries a first gas stream of unknown composition from, for example, a
18 process pipeline. Included along “stream 1” are pressure regulator 214 and pressure gage 215, shut-
19 off valve 216, particulate filter 217, and a first stream switching valve 218. Second pipe or tube 220
20 connects to a second sample point 222 and carries second gas stream of unknown composition.
21 Included along “stream 2” are pressure regulator 224 and pressure gage 225, shut-off valve 226,
22 particulate filter 227, and a second stream switching valve 228. The third pipe or tube 230 connects
23 to a third sample point 232 and a calibration sample of known composition. Included along the

1 third path are pressure regulator 234 and pressure gage 235, shut-off valve 236, particulate filter
2 237, and a third switching valve 238. Third switching valve 238 connects not only to filter 237,
3 through one port, but also to first and second switching valves 218, 228 through another. Yet
4 another port of third switching valve 238 attaches to regulator 240 and flow meter 245. Flow meter
5 245 attaches through a relatively long tube to sample shut-off valve 255 housed in analyzer oven
6 250. Sample valve 255 connects to a sample valve in the oven, and then connects to the vent 260.
7 As can be appreciated, although only two streams of unknown fluids are shown, additional streams
8 could be added by the use of a greater number of flow paths.

9 During operation, a gas chromatograph housed in analyzer oven 250 is calibrated using the
10 calibration sample from sample point 232. The pressure and flow rate of this stream are maintained
11 by pressure regulator 234, regulator 240 and flow meter 245. Because the composition of the
12 calibration sample is known, it may be used to calibrate the gas chromatograph. The calibration
13 sample flows through third switching valve 238, through the gas chromatograph 150 and out sample
14 vent 260. If a measurement of the fluid at sample point 222 is desired, the gas along the second pipe
15 is allowed to flow by actuation of second stream switching valve 228, through first stream switching
16 valve 218, and through third stream switching valve 238. The third switching valve 238 is the only
17 valve in the stream switching system that on its own can prevent or block the flow of fluid from all
18 the sample points. Thus, this configuration is referred to as a "single block" stream switching
19 system. One drawback of this design is that the fluid from sample point 222 flows through all of the
20 first, second, and third switching valves prior to arrival at the gas chromatograph, and malfunction
21 of only a single one of these switching valves prevents the measurement of a sample of fluid from
22 stream 2.

1 If, after the above-described measurement of stream 2, it is desired to measure the fluid from
2 stream 1, the system must be purged of the previous fluid sample. Purging of the old fluid stream
3 from the system prevents contamination between the streams. Thus, the stream switching system of
4 Figure 2 would switch from stream 2 to stream 1. At that time, adequate accuracy by the gas
5 chromatograph has likely been assured if all the other necessary criteria have been met. Many refer
6 to a configuration having a single sample vent as a "single bleed" stream switching system.

7 Thus, a "dead volume" of fluid in a stream switching system is a significant problem.
8 Another problem encountered in a stream switching system is the reliability and maintenance of the
9 system. Because an operator may visit a particular stream switching system only infrequently, the
10 system should be accurate, reliable, as immune to breakdown as possible, and simple to repair when
11 problems do occur. This highly sought after combination of features is not available with current
12 stream switching systems.

13 Another drawback in many prior systems is their difficulty in analyzing a complex fluids
14 because of limitations in the associated gas chromatographs. It would be desirable if a stream
15 switching system could be developed that could quickly transfer fluid sample to the analyzer. This
16 drawback also reduces the usefulness of a stream sampling system.

17 A stream sampling system is needed that is faster, more reliable, more flexible, and more
18 accurate than previous stream sampling systems. Ideally, such a stream sampling system could
19 reduce the adverse effects of "dead volume." This ideal stream sampling system would also be less
20 prone to breakdown than previous models, while providing much faster and more accurate
21 measurements.

22

SUMMARY OF THE INVENTION

The invention features a stream switching system including a housing having a common stream path with multiple input ports and at least one output port, tubing connected to the output port, the tubing including a heating coil to heat and control the flow rate of a fluid sample traveling through the heating coil. An insulated housing encapsulating the stream switching housing may be included to stabilize the temperature of the stream switching housing. A silicone rubber heater may also be attached to the stream handling housing. Numerous solenoids or other fluid flow activation switches also connect to the stream switching housing and preferably are positioned outside of the insulated housing.

Another inventive feature of the stream switching system is the use of fluid flow switches (such as solenoids attached to a pressurized line) that prevent the flow of gas while an outside impulse is being applied. This prevents stream switching system leakage during, for example, power failure. The invention also includes a stream switching system having a sample point, a stream switching portion, tubing connecting the two, and one or more membrane or cartridge filters located proximate (preferably within 10 feet and even more preferably within 3 feet) the sample point.

Thus, the invention comprises a combination of features and advantages which enable it to overcome various problems of prior devices. The various characteristics described above, as well as other features, will be readily apparent to those skilled in the art upon reading the following detailed description of the preferred embodiments of the invention, and by referring to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

For a more detailed description of the preferred embodiment of the present invention, reference will now be made to the accompanying drawings, wherein:

Figure 1 is a prior art sample handling system.

Figure 2 is a prior art stream switching system.

Figure 3 is a schematic of a stream switching system according to an embodiment of the invention.

Figure 4 is an exploded side view of the embodiment of Figure 3.

Figure 5 is a magnified view of Figure 4.

Figure 6 is an improved sample handling system according to an embodiment of the invention.

Figure 7 is an improved stream switching system according to another embodiment of the invention.

Figure 8 is a preferred embodiment of the stream switching system of Figure 7.

Figure 9 is a preferred Division 1 implementation of the stream switching system of Figure

Figure 10A is a top view of a Division 1 solenoid manifold.

Figure 10B is a side view of a Division 1 solenoid manifold.

Figure 11A is a top view of a Division 1 manifold.

Figure 11B is a side view of a Division 1 manifold.

Figure 12 is a preferred Division 2 implementation of the stream handling system of Figure

Figure 13 is a top view of a Division 2 manifold.

1 Figure 14 is a top view of a Division 2 bottom insulator.

2 Figure 15A is a top view of a Division 2 solenoid manifold.

3 Figure 15B is a side view of a Division 2 solenoid manifold.

4 Figure 16 is a prior art sample handling system.

5

6 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

7 Figure 3 shows a “double block and double bleed” of one preferred embodiment of a stream
8 switching system according to the invention. The stream switching system 300 includes four
9 streams upstream of a stream handling portion 391. Four streams include a calibration sample 301,
10 stream 1 302 corresponding to a first fluid sample, stream 2 303 corresponding to a second fluid
11 sample, and stream 3 304 corresponding to a third fluid sample. It is to be understood that more or
12 fewer ports can be included and that one or more separate stream switch systems could be included.

13 Streams 301-304 supply various fluid samples to the sample wetted portion, and connect
14 respectively to actuatable calibration port 311 and actuatable stream ports 312-314. Actuatable
15 ports 315-316 and 332-333, as well as ports 331 and 334, are also part of the sample wetted portion
16 391. Each actuatable port may be actuated into either an open or closed state as controlled by eight
17 connected solenoids 350-357 (also labeled SV1-SV8) which correspond respectively to ports 311-
18 316, 332-333. When a port is in an open state, fluid may pass freely through the port. When a port
19 is in a closed state, fluid is prevented from flowing through that port. Also shown in Figure 3 are
20 solenoid pressure line 358 and solenoid vent line 359, as well as gas path 342 extending from port
21 315 to ports 333 and 332.

22 As explained further below, each actuatable stream port 312-314, as well as actuatable
23 calibration port 311, is positioned in an area 320 that creates a common sample path. Also

1 positioned in the common sample path 320 are an actuatable “blocking” port 315 and an actuatable
2 “bleed” port 316. In addition, area 321 creates a first sample shut off that contains two “blocking”
3 ports 332 and port 331. Area 322 creates a second sample shut off that contains two “blocking”
4 ports 333 and port 334. As shown, ports 332 and 333 are actuatable, while ports 331 and 334 are
5 not. It is to be understood, however, that all of these ports could be actuatable, or that ports 332 and
6 333 could be actuatable while ports 331 and 334 are not.

7 Two channels, channel 1 340 and channel 2 345, are output tubing that direct fluid sample
8 away from the stream switching system. As used with reference to the invention, the term tubing is
9 used in a general manner and includes other fluid transportation mediums such as piping. The
10 channels connect to, for example, downstream gas chromatographs including valve, heating, and
11 measurement devices. Each channel thus may be separately analyzed by a gas chromatograph.
12 Each channel can also be used as a flow path to “bleed” the system when switching from sample
13 point to sample point.

14 As can also be appreciated, first and second sample shut offs correspond to first and second
15 channels 340, 345. Consequently each channel is associated with two solenoids 350 and 357, either
16 one of which can be actuated to prevent the flow of any fluid through the channel. It can be
17 appreciated that the use of a solenoid to prevent the flow of fluid is not absolutely necessary, and
18 any suitable mechanical or electrical gas flow actuation switch may be used. In the illustrated
19 embodiment, the flow of fluid through channel 1 may be prevented by closing either actuatable
20 blocking port 315 or actuatable port 332 in the first sample shut off. Similarly, the flow of fluid
21 through channel 2 may be prevented by closing either actuatable blocking port 315 or the actuatable
22 port 333 in the second sample shut off. Thus, because the flow of fluid may be prevented through a
23 channel at either of two locations, this is a “double block” design. In addition, the system may be

1 bled through sample bleed port 316. Thus, because the system may be bled either through a channel
2 or through the sample bleed port 316 the embodiment is a “double bleed” design.

3 Referring now to Figure 4, a side exploded view of the stream switching portion 391 is
4 shown. In this embodiment, the stream switching portion constitutes upper, middle, and lower
5 plates aligned and connected together by dowel pins 470 and torque screws 471-475. The lower
6 plate, referred to as a manifold plate 410, includes eight actuation ports 411-418 connected by
7 tubing to solenoids 350-357 (not explicitly shown in Figure 4). The middle plate, also called a
8 piston plate 420, includes eight locations 421-428 designed to receive respective pistons 450-457.
9 Middle plate 420 also includes shallow channels, chambers, or grooves that form areas 320-322, as
10 described with reference to Figure 3. The upper plate, referred to as the primary plate 430, includes
11 screw holes corresponding to the torque screws, as well as three exemplary fluid ports 316, 332, and
12 331. Eight pistons 450-457 (corresponding to ports 311-316, 332-333) as well as a pair of actuating
13 diaphragms 440 lie between manifold plate 410 and middle plate 420. Sealing diaphragm 465 and
14 cushion diaphragm 460 lie between the primary plate 430 and middle plate 420. These diaphragms
15 ensure a leak-free fit between each pair of plates and between a piston and its corresponding port.
16 The actuating diaphragms may be made from Kapton of about 3 mm thickness. Similarly, the
17 sealing diaphragms may be made from Teflon coated Kapton. However, as would be appreciated
18 by those of ordinary skill, the invention is not limited solely to these sealing diaphragms.

19 Figure 5 includes a close-up view of piston 454, manifold plate 410 with attached solenoid
20 or other appropriate fluid flow activation switch, middle plate 420, primary plate 430 including
21 passage 530 (corresponding to one of the ports illustrated in Figures 3 and 4), and diaphragms 440,
22 460, and 465. The left portion of Figure 5 includes a fluid stream 510 such as a calibration gas or
23 fluid sample. The right portion of Figure 5 includes actuation gas 520. When a port is open (as

1 shown on the left side of Figure 5), a fluid stream 510 between primary plate 430 and diaphragm
2 465 exits through passage 530. Conversely, when a port is closed (as shown on the right), there is
3 no flow of a fluid stream 510. Instead, an actuation gas 520 is applied by the solenoid 525 against
4 the piston head of piston 454. The piston 454 is forced upward, with its narrow end abutting the
5 lower end of passage 530 formed in primary plate 430. Because the relatively large surface area of
6 its head is presented to the actuating fluid 520, the piston 454 inherently multiplies the force
7 available such that a gas tight seal is formed against the passage 530. As can be appreciated, a
8 piston is not the only possible actuation member, with suitable devices including solenoids, flapper
9 valves, direct diaphragm valves, and others.

10 Referring to Figures 3, a sample from stream 1 302 will be used to illustrate the operation of
11 the device. The pressure in each stream from a pipeline is normally reduced to about 15-25 psi.
12 Consequently, a sample from, for example, a process pipeline travels to channel 320 via port 312
13 when port 312 is open. Port 312 being open corresponds to piston 454 being in a lower position.
14 As can be understood from Figure 4 and as is shown in Figure 5, the piston 454 is forced to this
15 lower position from the fluid pressure applied through stream 1 302 and a lack of actuation pressure
16 applied by solenoid 354. Gravity may also assist in the piston falling to a lower position. To avoid
17 cross-contamination, when port 312 is open, ports 311, 313, and 314 are, therefore, closed in normal
18 operation. This closure of ports 311, 313, and 314 corresponds to pistons 455, 453 and 452 being in
19 an elevated position by activation fluid pressure applied through solenoids 355, 353 and 352. As
20 can consequently be appreciated, the assembly shown in Figure 4 need not be vertical, but instead
21 can operate from a variety of angles, and the use of terms such as "lower" and "upper" is merely for
22 explanatory purposes.

1 The fluid sample travels through port 312 and along common stream channel 320 to
2 blocking port 315, which is also open by operation of the associated solenoid. The sample then
3 travels through blocking port 315 and along gas path 342 that includes a "T" at point 343. This "T"
4 intersection at point 343 splits the sample into two portions. A first portion travels to sample shut
5 off channel 321 via actuatable port 332. When port 332 is open, the sample travels along the
6 sample shut off channel to port 331, which then allows this first portion of the sample to flow out
7 channel 1 340 to a first gas chromatograph (not shown). A second portion of the sample travels to
8 sample shut off channel 322 via an open actuatable port 333. Port 334 allows this second portion of
9 the sample to flow out channel 2 345 to a second gas chromatograph (not shown). As would be
10 appreciated by one of ordinary skill in the art, gas path 342 may be external tubing or may be milled
11 into one or more plates, such as lines permanently drilled into primary plate 430.

12 The double block and double bleed design of this embodiment has particular advantages.
13 For example, when switching from stream 1 to stream 2, the system must be bled. First, the sample
14 shut offs are closed to block the flow stream by the closure of sample shut off ports 332 and 333 by
15 actuation of solenoids 350 and 357. Stream port 312 is also closed to block the flow of pressurized
16 gas from stream 1. A short time thereafter, sample bleed port 316 in the common stream path is
17 opened while port 315 is still open, allowing the pressurized gas in common stream path 320 to
18 equalize to atmospheric pressure. Simultaneously, inside the associated gas chromatograph 150, the
19 carrier gas associated with the well-known operation of the chromatographic valve sampling injects
20 an aliquot of sample fluid for analysis by the gas chromatograph. When this occurs, the remaining
21 fluid in the system downstream of the sample shut offs is allowed to equalize to atmospheric
22 pressure. At that time, the sample shut offs can be opened, the sample bleed port 316 closed, and
23 the system purged with the new stream from stream 2. Because the pressure of the stream switching

1 system has already been lowered to atmospheric pressure, and because stream 2 is under pressure,
2 the sample from stream 2 will quickly flow through the stream switching system. This results in a
3 faster purging with lower volumes of the new sample being necessary.

4 As an additional benefit to this embodiment, the use of two channels allow near-parallel
5 analysis by separate gas chromatographs or detectors within the same gas chromatograph, which
6 can speed the sample analysis of a complex sample having numerous components. For example, an
7 open first sample shut off and closed second sample shut off allows sample to flow through channel
8 1 for a period of five seconds. An open second sample shut off and closed first shut off could them
9 allow sample to flow through channel 2 for the next five seconds. This results in near-simultaneous
10 analysis by the gas chromatographs or detectors.

11 Moreover, this design is particularly desirable because the advantages recited above are
12 achieved without the expense otherwise necessary (such as for extra valves, etc) to attain a double
13 block and double bleed configuration. Further, the above design can be easily modified for
14 particular situations. For example, additional ports can be freed for use as stream ports if only
15 single blocking or only a single channel is desired. The design can also be modified to be a single
16 bleed design, if desired. The design may also be modified to add or subtract parts as necessary.

17 Improvements to this design are also possible. For example, it is known to modify the
18 design of Figure 2 to include membrane filters that by-pass liquid condensate as shown in Figure 16.
19 Membrane filters prevent condensate in the pipeline from flowing into the stream switching system,
20 which can contaminate the gas chromatograph.

21 Figure 16 includes a stream switching system attached to an analyzer oven 1650 that is part
22 of gas chromatograph 150. Three input pipes or tubes 1610, 1620, 1630 attach to switching system
23 140, and correspond to first, second and third flow paths. The first pipe or tube 1610 connects to a

1 first sample point 1612 and carries a first fluid stream of unknown composition from, for example, a
2 process pipeline. Included along "stream 1" are pressure regulator 1614 and pressure gage 1615,
3 shut-off valve 1616, particulate filter 1617, and a first stream switching valve 1618. Interposed
4 between particulate filter 1617 and first stream switching valve 1618 is membrane filter 1670.
5 Connected to membrane filter 1670 are flow meter 1671, valve 1672, and bypass line 1611 for
6 alternate expulsion of sample from "stream 1." Second pipe or tube 1620 connects to a second
7 sample point 1622 and carries second fluid stream of unknown composition. Included along
8 "stream 2" are pressure regulator 1624 and pressure gage 1625, shut-off valve 1626, particulate
9 filter 1627, and a second stream switching valve 1628. Interposed between particulate filter 1627
10 and first stream switching valve 1628 is membrane filter 1680. Connected to membrane filter 1680
11 are flow meter 1681, valve 1682, and bypass line 1621 for alternate expulsion of sample from
12 "stream 2." The third pipe or tube 1630 connects to a third sample point 1632 and a calibration gas
13 stream of known composition. Included along the third path are pressure regulator 1634 and
14 pressure gage 1635, shut-off valve 1636, particulate filter 1637, and a third switching valve 1638.
15 Third switching valve 1638 connects not only to filter 1637, through one port, but also to first and
16 second switching valves 1618, 1628 through another. Yet another port of third switching valve
17 1638 attaches to regulator 1640 and flow meter 1645. Flow meter 1645 attaches through a
18 relatively long tube to sample shut-off valve 1655 housed in analyzer oven 1650. Also connected to
19 sample shut-off valve 1655 is sample vent 1660. As can be appreciated, although only two streams
20 of unknown gas are shown, additional streams could be added by the use of a greater number of
21 flow paths. As can be appreciated, the membrane filters of Figure 16 are located close to the stream
22 switching valves. This location for the membrane filters eliminates liquid condensate from sample
23 immediately upstream from chromatograph sample valve, if desired.

1 The inventive arrangement of Figure 6 includes a sample point (preferably a probe) 615 that
2 is located at, for example, process pipeline 610. Attached to sample probe 615 is a sample flow
3 path that includes tubing or piping 620, a pressure regulator 625, pressure gage 630, regulator 635,
4 one or more membrane filters 640, heat tracing 645, valve 650, particulate filter 655, sample
5 switching system 660 including a flow resistor and pre-heat coil 661, and gas chromatograph 665.

6 As can be appreciated, in this embodiment the membrane filter(s) 640 are located not in the
7 sample switching system 660, but instead are located near the sample point. These filters are
8 preferably within ten feet, and even more preferably, within three feet of the sample point.
9 Placement of the membrane filters 640 as close to the sample point 610 as feasible results in a
10 number of advantages. For example, because every device in the stream has an associated pressure
11 drop, the closer the filter is to the sample point, the lower the pressure needed in the overall system
12 to force the sample through the filter. Therefore, the embodiment of Figure 6 has sufficient pressure
13 to force the sample gas through the membrane filter. In addition, membrane filters require
14 occasional replacement. Placement of the membrane filter close to the sample point, and the
15 accompanying lower pressure necessary to operate the system, results in a longer life filter. Further,
16 if and when the filter's operating life does expire, the location of the filter outside the stream
17 switching system simplifies replacement and maintenance. This location for the membrane filter
18 also simplifies the heating of the sample on the sample handling system, if desired. This design
19 change could also be applied to cartridge filters with a similar result.

20 Other improvements to the system include the manner of maintaining a target temperature
21 for a stream switching system. Often in previous systems, the stream switching portion of the
22 system was not heated. Even where this portion was heated, it was difficult to maintain a constant

1 temperature because of the large mass and size of the stream switching portion. In contrast, Figures
2 7-8 illustrate improvements to the stream switching system of Figures 3 and 4.

3 Figures 7-15B illustrate stream switching portions designed to maintain an elevated
4 temperature within a narrow range. Stream switching system 700 includes a flow panel portion 790
5 upstream of sample wetted portion 791. Flow panel portion includes inputs for calibration 701,
6 stream 1 702, stream 2 703, and stream 3 704. Streams 701-704 include respective valves 705 and
7 respective particulate filters 706 along each stream's length prior to entry of the sample wetted
8 portion of the stream switching system.

9 Streams 701-704 supply various fluid samples to the sample wetted portion, and connect
10 respectively to actuatable calibration port 711 and actuatable stream ports 712-714. Actuatable
11 ports 715-716 and 732-733, as well as ports 731 and 734, are also part of the sample wetted portion
12 791. Each actuatable port may be actuated into either an open or closed state as controlled by eight
13 connected solenoids 750-757 (SV1 - SV8) which correspond respectively to ports 711-716, 732-
14 733. When a port is in an open state, fluid may pass freely through the port. When a port is in a
15 closed state, fluid is prevented from flowing through that port. Also shown in Figure 7 are solenoid
16 pressure line 758 and solenoid vent line 759.

17 As is explained further below, each actuatable stream port 712-714, as well as actuatable
18 calibration port 711, is positioned in an area 720 that creates a common sample path. Also
19 positioned in the common sample path 720 are an actuatable "blocking" port 715 and an actuatable
20 "bleed" port 716. In addition, area 721 creates a first sample shut off that contains tube "blocking"
21 ports 732 and 731. Area 722 creates a second sample shut off that contains two "blocking" ports
22 733, and port 734. As shown, ports 732 and 733 are actuatable, while ports 731 and 734 are not. It

1 is to be understood that all of these ports could be actuatable, or ports 731 and 734 could be
2 actuatable while ports 732 and 733 are not.

3 Two channels, channel 1 740 and channel 2 745, are output tubing that direct fluid sample
4 away from the stream switching portion. A first flow restrictor and pre-heat coil 760 is in
5 association with coil 1, and a second flow restrictor and preheat coil 761 is in association with coil
6 2. More specifically, first pre-heat coil 760 is located between "T" point 743 and the first sample
7 shut off. Second pre-heat coil 761 is located between "T" point 743 and the second sample shut off.

8 This stream switching system operates in generally the same manner as the stream switching
9 system of Figure 3. However, as sample flows through the respective flow restrictors and pre-heat
10 coils 760, 761, the sample is heated. This heating of the sample, if desired, accomplishes two goals.
11 First, the sample must preferably be introduced to the gas chromatograph as a single phase sample
12 instead of a two-phase liquid/gas sample. Temperatures above about 80 degrees Fahrenheit are
13 normally adequate to maintain a gaseous sample of most hydrocarbon process streams at a sample
14 pressure of 15-25 psi. Second, an elevated temperature (preferably near the chromatograph
15 temperature) for the sample is desirable for the optimal operation of the gas chromatograph. Thus,
16 the "pre-heating" of the sample helps to achieve a more accurate measurement of the sample's
17 composition by the gas chromatograph. Further, the pre-heat coil additionally acts as a restriction
18 column to flow because of a small inner diameter. By selecting the proper diameter tubing, the
19 sample flow at the vent is reduced from an unobstructed 200-250 cc/minute at 15 psig inlet pressure
20 to about 50-70 cc/min at 15 psig. The increased control over sample flow rate given by the pre-heat
21 coil allows simultaneous analysis by gas chromatographs downstream to each coil.

22 An accompanying inventive feature is an insulative design that stabilizes temperature
23 variations in the stream switching system. The preferred insulative design changes depend on

1 whether the application is Division 1 or Division 2. A Division 1 application is in an area where the
2 hazard can exist under normal operating conditions. A Division 2 application is in area where
3 ignitable gases or vapors are handled, processed, or used, but which are normally closed containers
4 or closed systems from which they can only escape through accidental rupture or breakdown of
5 such containers or systems.

6 Figure 8 illustrates a stream switching system appropriate for Division 1 application. A
7 lower plate, referred to as a manifold plate 810, includes eight actuation ports. The middle plate,
8 also called a piston plate 820, includes eight locations designed to receive respective pistons 850-
9 857. Middle plate 820 also includes grooves, shallow channels or chambers that form areas 720-
10 722, as described with reference to Figure 7. The upper plate, referred to as the primary plate 830,
11 includes screw holes corresponding to torque screws, as well as fluid ports. Eight pistons 850-857
12 (corresponding to ports 711-716, 732-733) as well as a pair of actuating diaphragms 840 lie between
13 manifold plate 810 and middle plate 820. These diaphragms ensure a leak-free fit between each pair
14 of plates and between a piston and its corresponding port. The actuating diaphragm may be made
15 from Kapton of about 3 mm thickness. Sealing diaphragm 865 and cushion diaphragm 860 lie
16 between the primary plate 830 and middle plate 820. The sealing diaphragms may be made from
17 Teflon-coated Kapton. Supporting plate 880 attaches to and supports insulation plate 870, which in
18 turn attaches to the bottom of manifold plate 810.

19 Figure 9 includes the stream switching system 791 of Figures 7 and 8 in an insulative
20 housing. In order to stabilize the temperatures in heated zones, an "oven" is created from a thermal
21 insulation material. This oven is essentially a sleeve that surrounds the rest of the stream switching
22 system and keeps its temperature stable, except for the solenoids, which must be kept away from the
23 heat inside the oven. Insulation wall 910 surrounds stream switching system 791 and connects to

1 both bottom insulation 870 and to insulation cover 920. Attached to and supporting insulation cover
2 920 is upper supporting plate 930. Supporting plate 930 also attaches to solenoid manifold 940
3 which, in turn, connects to eight solenoids 950. Piping 960 connects solenoids 950 to manifold
4 plate 810. To simplify the illustration, only a single piping tube 960 is shown, but it is to be
5 understood that in the preferred embodiment each solenoid 950 connects via a separate piping to the
6 manifold plate 810. Also illustrated are tubing 970 attached to the stream switching system 791,
7 and one or more pre-heat coils 975, as explained with reference to Figure 7. One or more heaters
8 such as silicon rubber heaters may be located on the side of the stream switching system assembly
9 to warm and stabilize the temperature of stream switching system 791. Insulative housing is
10 preferably made from foam material, manufactured by and available from Rogers InC. The entire
11 assembly may be aligned by dowel pins and attached together by a plurality of screws that protrude
12 through the insulative housing. The assembly may then be located in an explosion-resistant
13 container suitable for the Division 1 environment.

14 Figures 10A and 10B show a Division 1 solenoid manifold 940. Solenoid manifold 940
15 includes eight regions 1011-1018 corresponding to eight solenoids. Each region 1011-1018
16 contains five holes corresponding to an input pressure line, a release line, an actuation gas line, and
17 two mounting holes. As shown in Figure 10B, the Division 1 solenoid manifold includes eight side
18 portals corresponding to the piping that connects the solenoid manifold 940 and the manifold plate
19 810. Holes 1020, 1025 are screw holes.

20 Figures 11A and 11B show a Division 1 manifold plate 810. Manifold plate 810 includes
21 ten screw holes 1110-1119 suitable for torque screws, and two dowel pin holes 1105, 1106. Gas
22 pressure from the solenoids travels through eight portals 1111-1118 to actuate the pistons.

1 Figure 12 illustrates a system containing a stream switching system appropriate for Division
2 2 application. This Division 2 system is typically wall mounted, and is divided into a lower
3 (sample) enclosure 1290 and an upper (electronics) enclosure 1295. Lower enclosure 1290 includes
4 a stream switching system 791 proximate to an opening in wall 1225. Stream switching system 791
5 attaches at its bottom to an insulator 1210. Insulator 1210, preferably made from Teflon, connects
6 to an outside manifold 1215. On its bottom, outside manifold 1215 contains eight pressure input
7 locations corresponding to the eight pistons of the stream switching system. The stream switching
8 system is encased in an insulation cover 1220 that is anchored to wall 1225. Also inside insulation
9 cover 1220 may be tubing 1270 or one or more heating coils. Upper enclosure 1295 includes a set
10 of solenoids 1250 attached to a solenoid manifold 1240 and outside solenoid manifold 1230. Piping
11 1260 connects outside solenoid manifold 1230 to outside manifold 1215. The Teflon insulator 1210
12 is a trademark of DuPont.

13 Figure 13 shows a Division 2 outside manifold 1215. Eight ports correspond to the eight
14 pistons of the preferred embodiment. Fourteen torque screw holes 1320-1333 for torque screws are
15 also shown, in addition to two dowel pin holes 1341, 1342 suitable for dowel pins.

16 Figure 14 shows a bottom insulator 1210 that connects to outside manifold 1215. Bottom
17 insulator 1210 includes eight through holes 1411-1418 for communicating gas pressure to the
18 pistons of the stream switching system. Fourteen torque screw holes 1420-1433 receive the same
19 torque screws as placed through the outside manifold 1215. Six through holes for tubing fitting
20 connection

21 Figures 15A and 15B show an upper or outer solenoid manifold 1230. Included are eight
22 regions 1511-1518 corresponding to eight solenoids. Each region 1511-1518 contains five holes

1 corresponding to an input pressure line, a release line, an actuation gas line, and two mounting
2 holes. Also shown are actuating gas supply line 1519 and vent line 1520.

3 Referring back to Figure 7, another improvement is the use of solenoids 750-757 to increase
4 safety. If conventional electronically-actuated solenoids are utilized with the stream switching
5 system of Figure 7, upon a power failure gas sample will flow freely through the sample handling
6 system, resulting in a risk of explosion and waste of gas. In the preferred embodiment, the solinoids
7 are also switched electronically. Under normal operating conditions, however, the solenoid used
8 with the invention is "open." When these solenoids 750-757 are open, actuating gas can flow into
9 the valve to push the pistons into an upper, elevated position, stopping sample flow. Thus, upon a
10 power failure or similar mishap, the solinoids 750-757 are open and the stream switching system of
11 Figure 7 will stop the sample flow. This significantly lessens the chance of explosion. These
12 solenoids "close" only upon the application of actuation gas from the pressure line, which requires
13 electrical power.

14 While preferred embodiments of this invention have been shown and described,
15 modifications thereof can be made by one skilled in the art without departing from the spirit or
16 teaching of this invention. The embodiments described herein are exemplary only and are not
17 limiting. Many variations and modifications of the system and apparatus are possible and are within
18 the scope of the invention. Accordingly, the scope of protection is not limited to the embodiments
19 described herein, but is only limited by the claims that follow, the scope of which shall include all
20 equivalents of the subject matter of the claims.

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